

OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT CALCULATION COVER SHEET

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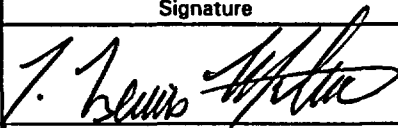

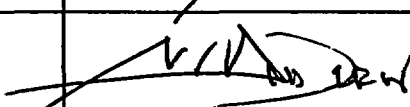
Of: 20

2. Calculation Title
Thermal Evaluation for the Naval SNF Waste Package

3. Document Identifier (including Revision Number)
CAL-VDC-TH-000001 REV 00

4. Total Attachments
22

5. Attachment Numbers - Number of pages in each
See block 9, Remarks

	Print Name	Signature	Date
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9. Remarks

Number of Pages in each Attachment:

I-2, II-4, III-3, IV-7, V-8, VI-8, VII-7, VIII-8, IX-8, X-7, XI-7, XII-7, XIII-7, XIV-8, XV-8, XVI-7, XVII-8, XVIII-8, XIX-7, XX-7, XXI-7, XXII-3.

Revision History

10. Revision No.	11. Description of Revision
00	Initial Issuance.

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1. PURPOSE

The purpose of this calculation is to evaluate the thermal performance of the naval long spent nuclear fuel (SNF) waste package (WP) under multiple disposal conditions in a monitored geologic repository (MGR). The scope of this calculation is limited to determination of thermal temperature profiles upon the surface of, and within, the naval long SNF WP. The objective is to develop a temperature profile history within the WP, at time increments up to 10,000 years of emplacement. The results of this calculation are intended to support the Naval SNF WP Analysis and Model Report (AMR) for Site Recommendation (SR). This calculation was performed to the specifications within its Technical Development Plan (TDP) (Ref. 8.16). This calculation is developed and documented in accordance with the AP-3.12Q / REV. 0 / ICN. 0 procedure, *Calculations*.

2. METHOD

The evaluation method to be employed is finite element analysis (FEA). The calculation is performed by representing a two-dimensional (2-D) cross section of the WP using the ANSYS code, as described in Section 4.1. The problem is solved parametrically for various WP spacing, with and without backfill, for 25 and 50 years of pre-closure ventilation, up to 10,000 years of repository emplacement using transient FEA.

3. ASSUMPTIONS

- 3.1 It is assumed that a 2-D finite element representation of the WP cross section midway along the axis will conservatively represent the WP by providing higher temperatures than would be expected in a 3-D representation. Inherent to this assumption is that axial heat transfer does not significantly affect the solution (i.e., the flow of heat in the radial direction is assumed to dominate the solution). The basis for this assumption is that the metal thermal conductivity and heat generation distributions are such that axial heat transfer is very small or negligible at the midsection. This assumption is used in Section 5.1.
- 3.2 Representing only conduction and radiation heat transfer inside the WP is assumed to provide conservative results (higher temperatures) for this calculation. The basis for this assumption is as follows. The fill gas placed inside the WP will allow natural convective heat transfer to exist; however, since the enclosed basket cavities are orientated perpendicular to the direction of gravity, convection cells of appreciable effect do not develop. Thus, the problem may be represented with only the dominant heat transfer modes, with a negligible and/or conservative impact upon the results. This assumption is used in Section 5.4.
- 3.3 The properties of helium at a pressure of one atmosphere is assumed to be representative of the conditions that it will experience in the WP. The basis for this assumption is the fact that a one-atmosphere fill pressure at ambient temperature is representative of industry standard for storage casks. Page 4 of Ref. 8.4 indicates that the highest pressure

to which storage casks are filled is approximately 1.5 atmosphere; also, most industry vendors use substantially lower pressure in their designs. Even though the internal pressure of the WP will increase due to the temperature rise, the thermal conductivity of most gases is pressure independent provided the mass density remains constant (Ref. 8.3, p. 255). Thus, using the thermal conductivity at one atmosphere is reasonable. This assumption is used in Section 5.2.

- 3.4 The volumetric heat generation rate of the canistered naval fuel is assumed homogenous over the cross section considered for the calculation. The basis for this assumption is lack of information concerning the radial variation of the heat generation rate, and it is beyond the scope of this calculation to consider such minor effects. This assumption is used in Section 5.3.1.
- 3.5 The calculation will represent half the WP cross section. The basis for this assumption is the following. The geometry of the cross section is symmetrical about the cutting planes of the representation. Therefore, the heat conduction paths will also be symmetrical, resulting in no heat conduction across the cutting planes. The radiative heat transfer across these cutting planes is assumed negligible relative to the radiative heat transfer in the rest of the cross section. This assumption is used in Section 5.4.
- 3.6 The decay heat output of the Naval SNF Canister beyond 250 years after reactor shutdown is assumed to remain constant at the 250-year value of the design basis reactor. The U.S. Navy has not provided the values for reactor heat output beyond 250 years. The basis for this assumption is to show the Naval SNF WP provides appropriate internal and external temperatures for the Naval SNF Canister under conditions that bound all expected. This assumption is used in Section 5.1.
- 3.7 The U.S. Navy has provided a lumped set of thermal values for Naval SNF Canister. It is assumed these values when smeared over the internal volume of the Naval SNF Canister accurately represent the actual thermal performance of the Naval SNF Canister. The basis for this assumption is necessity. No other information is available for the Naval SNF Canister. This assumption is used in Section 5.1.
- 3.8 The U.S. Navy has provided a range of densities for the Naval SNF Canister. It is assumed the highest density value will bound all others for thermal storage. The basis for this assumption is to show temperatures for the surface of the Naval SNF Canister under conditions that bound all expected. This assumption is used in Section 5.1.
- 3.9 The Navy canister is assumed centered within the WP. The basis for this assumption is to simplify the representation and create the most thermally limiting configuration of components, ensuring that the model will give the highest possible temperatures within the WP. This assumption is used in Section 5.4.

- 3.10 The emissivity of stainless steel 316NG (nuclear grade) is assumed to be 0.60. The basis for this assumption is consistency with the range of emissivity for 316/316L material (0.57-0.66) given on p. 4-68 of Ref. 8.5. This assumption is used in Section 5.2.
- 3.11 The boundary temperature history for a Naval Canistered Fuel WP is assumed to be bounded by the boundary temperature history for the design basis 21 pressurized water reactor (PWR) WP given in Attachments 1 through 10 and 13 through 20 of Ref. 8.6. The boundary temperature history for this WP is given for various WP spacing, with and without backfill, for 25 and 50 years of pre-closure ventilation, up to 10,000 years of repository emplacement. The basis for this assumption is that the 21 PWR WP has a smaller diameter (1.564 m) and a higher heat generation rate (11.8 kW maximum), providing conservative temperatures within the WP. This assumption is used in Section 5.3.2.

4. USE OF COMPUTER SOFTWARE AND MODELS

4.1 SOFTWARE APPROVED FOR QUALITY ASSURANCE (QA) WORK

The FEA computer code used for this calculation is ANSYS Version (V) 5.4, which is identified by the Computer Software Configuration Item (CSCI) 30040 V5.4 and was obtained from Software Configuration Management in accordance with appropriate procedures. ANSYS V5.4 will hereafter be referred to as 'ANSYS.' ANSYS is a commercially available finite element thermal and mechanical analysis code and is appropriate for the thermal analysis of WPs, WP emplacements, and WP environments as utilized in this calculation.

The analyses using the ANSYS software were executed on a Hewlett-Packard J2240 workstation. The software qualification of the ANSYS software, including problems of the type analyzed in this calculation, is summarized in the *Software Qualification Report for ANSYS Version 5.4* (Refs. 8.7, 8.8, and 8.9). The ANSYS evaluations performed for this calculation are fully within the range of the validation for the ANSYS code used. Access to and use of the code for the calculation was granted and performed in accordance with appropriate procedures. Inputs to the ANSYS software are included as attachments and described in this calculation.

4.2 SOFTWARE ROUTINES

No software routines were used in the generation of this calculation.

4.3 MODELS

None used.

5. CALCULATION

The number of digits in the values cited herein may be the result of a calculation or may reflect the input from another source; consequently, the number of digits should not be interpreted as an indication of accuracy.

5.1 WASTE PACKAGE PROPERTIES

The naval WP represented in this calculation contains a single naval Long SNF Canister. The WP cross section studied in this calculation consists of the inner barriers, outer barriers, and the naval Long SNF Canister. This WP is modeled in two dimensions (see Assumption 3.1).

Table 1 lists the materials used in this calculation and their Unified Numbering System (UNS) designations.

Table 1. Materials Used and Their UNS Designations

Material Used	UNS Designation
Alloy 22	SB-575 N06022
Stainless Steel 316	SA-240 S31600
Helium	N/A

NOTE: N/A – not applicable

The naval canister geometry and materials used in this calculation are sketched in Attachment I. All properties of the naval fuel are assumed to be homogenous over the interior volume of the canister (Assumptions 3.6 through 3.8).

5.2 THERMAL PROPERTIES

Table 2 lists the density (Ref. 8.14, p. 7) and emissivity (Ref. 8.5, p. 4-68) of stainless steel 316. The emissivity is listed in Table 2 consistent with Assumption 3.10. The emissivity for the naval canister is 0.60 as specified by the U.S. Navy in Ref. 8.10, Enclosure 1, Page 4. Table 3 lists the thermal conductivity and specific heat of stainless steel 316. Values for thermal conductivity and thermal diffusivity are taken from Table TCD, Section II, of Ref. 8.12, and are converted here to conductivity and specific heat in SI units. The conversion of thermal diffusivity (defined in equation 1) to specific heat requires the density listed in Table 2. Stainless steel 316 is listed in the reference by its chemical composition (16Cr-12Ni-2Mo).

$$\text{Specific Heat (Btu/lb}\cdot^{\circ}\text{F)} = \frac{\text{Thermal Conductivity (Btu/hr}\cdot\text{ft}\cdot^{\circ}\text{F)}}{\text{Density (lb/ft}^3\text{)} * \text{Thermal Diffusivity (ft}^2\text{/hr)}} \quad (\text{Equation 1})$$

Table 2. Thermal Properties of Stainless Steel 316

Material	Density (kg/m ³)	Emissivity
Stainless Steel 316	7980	0.60

Table 3. Thermal Properties of Stainless Steel 316

Temperature		Thermal Conductivity (Btu/hr-ft-°F)	Thermal Diffusivity (ft ² /hr)	Thermal Conductivity (W/m-K)	Specific Heat (J/kg-K)
(°F)	(°C)				
70	21.11	7.7	0.134	13.33	482.93
100	37.78	7.9	0.136	13.67	488.19
150	65.56	8.2	0.138	14.19	499.38
200	93.33	8.4	0.141	14.54	500.68
250	121.11	8.7	0.143	15.06	511.31
300	148.89	9.0	0.145	15.58	521.64
350	176.67	9.2	0.148	15.92	522.43
400	204.44	9.5	0.151	16.44	528.74
450	232.22	9.8	0.153	16.96	538.31
500	260.00	10.0	0.156	17.31	538.73
550	287.78	10.3	0.159	17.83	544.43
600	315.56	10.5	0.162	18.17	544.72
650	343.33	10.7	0.164	18.52	548.33
700	371.11	11.0	0.167	19.04	553.57
750	398.89	11.2	0.170	19.38	553.69
800	426.67	11.5	0.173	19.90	558.66
850	454.44	11.7	0.176	20.25	558.69
900	482.22	12.0	0.178	20.77	566.58
950	510.00	12.2	0.181	21.11	566.47
1000	537.78	12.4	0.184	21.46	566.37
1050	565.56	12.7	0.186	21.98	573.84
1100	593.33	12.9	0.189	22.33	573.62
1150	621.11	13.1	0.191	22.67	576.42
1200	648.89	13.3	0.194	23.02	576.17
1250	676.67	13.6	0.196	23.54	583.15
1300	704.44	13.8	0.199	23.88	582.81
1350	732.22	14.0	0.201	24.23	585.37
1400	760.00	14.2	0.203	24.58	587.88
1450	787.78	14.4	0.206	24.92	587.48
1500	815.56	14.6	0.208	25.27	589.91

Table 4 lists the density of helium. Helium is used for the WP fill gas. The density is taken at one-atmosphere pressure (see Assumption 3.3) and a temperature of 300 K. Table 5 lists the thermal conductivity and specific heat of helium. All helium property values are taken from p. 759 of Ref. 8.11.

Table 4. Density of Helium

Material	Density (kg/m ³)
Helium (1 atm, 300 K)	0.1625

Table 5. Thermal Conductivity and Specific Heat of Helium

Temperature		Helium Thermal Conductivity (W/m·K)	Helium Specific Heat (J/kg·K)
(K)	(°C)		
260	-13.15	0.137	5193.0
280	6.85	0.145	5193.0
300	26.85	0.152	5193.0
350	76.85	0.170	5193.0
400	126.85	0.187	5193.0
450	176.85	0.204	5193.0
500	226.85	0.220	5193.0
550	276.85	0.236 ^a	5193.0
600	326.85	0.252	5193.0
650	376.85	0.264	5193.0
700	426.85	0.278	5193.0
750	476.85	0.291	5193.0
800	526.85	0.304	5193.0
900	626.85	0.330	5193.0
1000	726.85	0.354	5193.0

NOTE: ^a Linearly interpolated from the data supplied in the reference.

Table 6 lists the density and emissivity, and Table 7 lists the thermal conductivity and specific heat, of Alloy 22 used for the WP corrosion resistant barrier (inner barrier). The emissivity of Alloy 22 is taken from p. 10-297 of Ref. 8.13, as that of nickel-chromium alloy. The density, thermal conductivity, and specific heat are taken from p. 13 of Ref. 8.15.

Table 6. Density and Emissivity of Alloy 22

Material	Density (kg/m ³)	Emissivity
Alloy 22	8690	0.87

Table 7. Thermal Conductivity and Specific Heat of Alloy 22

Temperature (°C)	Thermal Conductivity (W/m·K)	Temperature (°C)	Specific Heat (J/kg·K)
48	10.1	52	414
100	11.1	100	423
200	13.4	200	444
300	15.5	300	460
400	17.5	400	476
500	19.5	500	485
600	21.3	600	514

5.3 WASTE PACKAGE HEAT OUTPUT AND BOUNDARY CONDITIONS

5.3.1 Waste Package Heat Output

Table 8 lists the heat output versus time for the naval SNF Canister. The values in Table 8 assume a homogeneous heat generation rate in the SNF cross-section (Assumption 3.4). The heat output applied to the finite element representation is from a design basis heat generation table provided by the U.S. Navy in Ref. 8.10.

Table 8. Heat Output of Naval SNF Canister

Time from Reactor Shutdown (years)	Heat Output (W)	Time from Reactor Shutdown (years)	Heat Output (W)	Time from Reactor Shutdown (years)	Heat Output (W)
0	8010	60	1770	600	30
1.0	7330	70	1410	700	30
2.0	6880	80	1120	800	30
3.0	6540	90	890	900	30
4.0	6280	100	710	1000	30
5.0	6050	110	570	2000	30
6.0	5850	120	450	3000	30
7.0	5680	130	360	4000	30
8.0	5530	140	280	5000	30
9.0	5400	170	150	6000	30
10	5290	195	90	7000	30
20	4250	241	30	8000	30
30	3430	300	30	9000	30
40	2760	400	30	10000	30
50	2210	500	30		

5.3.2 Waste Package Boundary Conditions

The boundary temperature histories applied in this calculation are those given in Attachments IV through XXI (attachments 1 through 10 and 13 through 20 of Ref. 8.6) for a design basis 21 PWR WP. The 21 PWR WP has a smaller outer diameter (1.564 m vs. 1.869 m) and a higher

initial heat generation rate (11.8 kW vs. 8.01 kW) than the naval long WP. Therefore, the design basis 21 PWR boundary temperature history will bound the naval long WP boundary temperature history (Assumption 3.11).

5.4 FINITE ELEMENT REPRESENTATION DEVELOPMENT

The temperature histories for 6 node locations within the WP were calculated. The peak temperature results and the time of peak temperature within the finite element representation are given in Table 11. The following simplifying assumptions were used in development of the finite element representation: Assumptions 3.2, 3.5, and 3.9.

Table 9 lists the accepted data used in this calculation, along with the pages in this document on which the actual values are listed. The data are considered accepted by virtue of the fact that the references from which they came are widely recognized engineering handbooks.

Table 9. Accepted Data Used in this Calculation

Data	Page	Accepted Reference
Density of stainless steel 316	9	8.14
Emissivity of stainless steel 316	9	8.5
Thermal conductivity and specific heat of stainless steel 316	10	8.12
Emissivity of Alloy 22	11	8.13
Density of helium	11	8.11
Specific heat of helium	11	8.11

6. RESULTS

This document may be affected by technical product input information that requires confirmation. Any changes to the document that may occur as a result of completing the confirmation activities will be reflected in subsequent revisions. The status of the input information quality may be confirmed by review of the Document Input Reference System database.

The results provided in this section are derived from the ANSYS executions. These calculations are presented in the output files of Ref. 8.2 (a compact disc [CD]). The input files for each of these calculations is provided as part of the output file. Table 10 is the list of files on the CD in Ref. 8.2.

Table 10. Output File Listing for Reference 8.2

File Name	File Description	Size	Date
Bf_0.1_25.out	With backfill, 0.1m WP spacing, 25-yrs. ventilation	775 kb	31 Jan 2000
NoBf_0.1_25.out	No backfill, 0.1m WP spacing, 25-yrs. ventilation	886 kb	31 Jan 2000
Bf_0.1_50.out	With backfill, 0.1m WP spacing, 50-yrs. ventilation	812 kb	31 Jan 2000
NoBf_0.1_50.out	No backfill, 0.1m WP spacing, 50-yrs. ventilation	865 kb	31 Jan 2000
Bf_0.5_50.out	With backfill, 0.5m WP spacing, 50-yrs. ventilation	811 kb	31 Jan 2000
NoBf_0.5_50.out	No backfill, 0.5m WP spacing, 50-yrs. ventilation	859 kb	31 Jan 2000
Bf_1.0_25.out	With backfill, 1.0m WP spacing, 25-yrs. ventilation	812 kb	31 Jan 2000
NoBf_1.0_25.out	No backfill, 1.0m WP spacing, 25-yrs. ventilation	896 kb	31 Jan 2000
Bf_1.0_50.out	With backfill, 1.0m WP spacing, 50-yrs. ventilation	841 kb	31 Jan 2000
NoBf_1.0_50.out	No backfill, 1.0m WP spacing, 50-yrs. ventilation	891 kb	31 Jan 2000
Bf_1.5_50.out	With backfill, 1.5m WP spacing, 50-yrs. ventilation	815 kb	31 Jan 2000
NoBf_1.5_50.out	No backfill, 1.5m WP spacing, 50-yrs. ventilation	879 kb	31 Jan 2000
Bf_2.0_25.out	With backfill, 2.0m WP spacing, 25-yrs. ventilation	800 kb	31 Jan 2000
NoBf_2.0_25.out	No backfill, 2.0m WP spacing, 25-yrs. ventilation	888 kb	31 Jan 2000
Bf_5.0_25.out	With backfill, 5.0m WP spacing, 25-yrs. ventilation	883 kb	31 Jan 2000
NoBf_5.0_25.out	No backfill, 5.0m WP spacing, 25-yrs. ventilation	870 kb	31 Jan 2000
Bf_10.0_25.out	With backfill, 10.0m WP spacing, 25-yrs. ventilation	866 kb	31 Jan 2000
NoBf_10.0_25.out	No backfill, 10.0m WP spacing, 25-yrs. ventilation	899 kb	31 Jan 2000

Table 11 contains the peak temperature profiles for the naval SNF canister and the WP.

Table 11. Peak Temperature Profiles Within the Naval Long WP

Filename	Time of Peak Temperature from Emplacement (years)	Temp. at Center of Naval Canister (°C)	Temp. at Inside of Naval Canister Shell (°C)	Temp. at Surface of Naval Canister (°C)	Temp. at Inside of Naval WP Inner Shell (°C)	Temp. at Interface Between WP Shells (°C)	Temp. at Surface of Naval WP (°C)
Bf_0.1_25.out	30	415.1	401.3	401.1	397.2	396.7	396.5
NoBf_0.1_25.out	40	250.6	238.3	238.1	232.9	232.6	232.4
Bf_0.1_50.out	60	306.0	299.0	298.9	295.4	295.0	294.9
NoBf_0.1_50.out	60	195.0	186.2	186.1	181.9	181.7	181.6
Bf_0.5_50.out	60	288.2	281.2	281.1	277.4	277.1	276.9
NoBf_0.5_50.out	60	186.4	177.3	177.2	173.0	172.7	172.6
Bf_1.0_25.out	30	364.1	350.5	350.3	345.5	345.0	344.8
NoBf_1.0_25.out	30 ^a	225.8	211.4	211.3	205.6	205.2	205.1
Bf_1.0_50.out	60	269.6	262.5	262.4	258.4	258.1	257.9
NoBf_1.0_50.out	60	176.6	167.5	167.4	163.0	162.8	162.7
Bf_1.5_50.out	60	254.4	247.0	246.9	242.7	242.3	242.2
NoBf_1.5_50.out	60	169.0	159.7	159.6	155.1	154.9	154.8
Bf_2.0_25.out	30	324.6	310.9	310.7	305.2	304.7	304.5
NoBf_2.0_25.out	30 ^b	209.2	192.7	192.5	186.2	185.8	185.7
Bf_5.0_25.out	30	260.7	246.5	246.3	239.1	238.6	238.4
NoBf_5.0_25.out	30	186.6	169.4	169.2	160.9	160.5	160.3
Bf_10.0_25.out	30	222.0	206.4	206.2	197.6	197.0	196.7
NoBf_10.0_25.out	30	180.0	162.5	162.2	153.6	153.2	153.0

^a Time for center temperature, 40 years for all other temperatures.

^b 30 years for center, inside and surface of naval canister temperature, 40 years for all other temperatures.

Figure 1 graphs the temperature profiles for the no-backfill cases with 25 years of pre-closure ventilation given in Tables 11. Note that the peak temperature times differ.

Figure 2 graphs the temperature profiles for the no-backfill cases with 50 years of pre-closure ventilation given in Tables 11. Note that the peak temperature times differ.

Figure 3 graphs the temperature profiles for the backfill cases with 25 years of pre-closure ventilation given in Tables 11. Note that the peak temperature times differ.

Figure 4 graphs the temperature profiles for the backfill cases with 50 years of pre-closure ventilation given in Tables 11. Note that the peak temperature times differ.

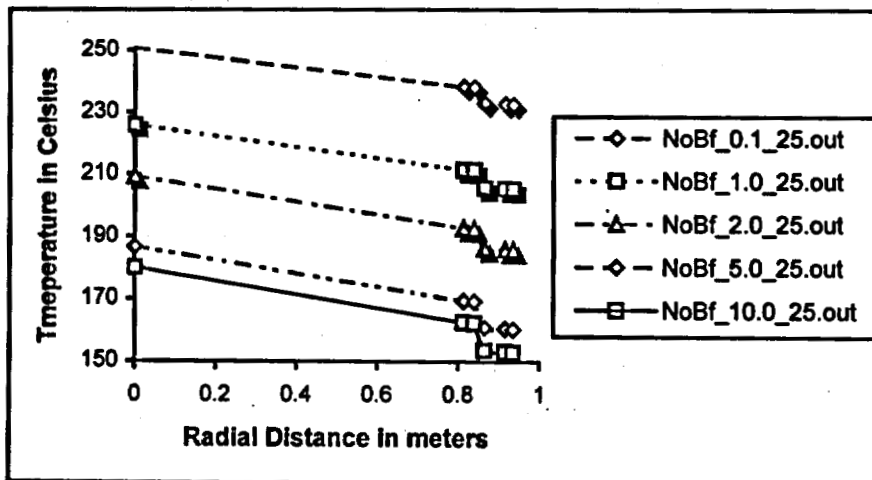


Figure 1. Temperature Versus Radial Distance for the Cases Without Backfill (25-yr. ventilation)

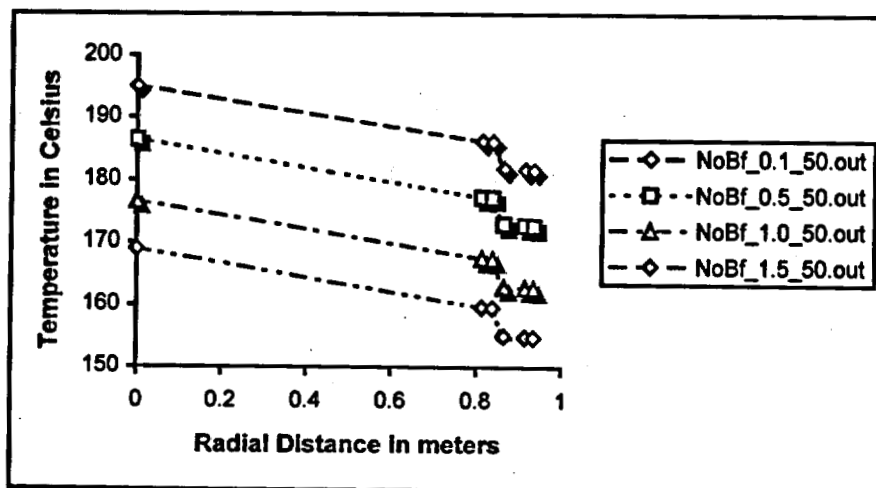


Figure 2. Temperature Versus Radial Distance for the Cases Without Backfill (50-yr. ventilation)

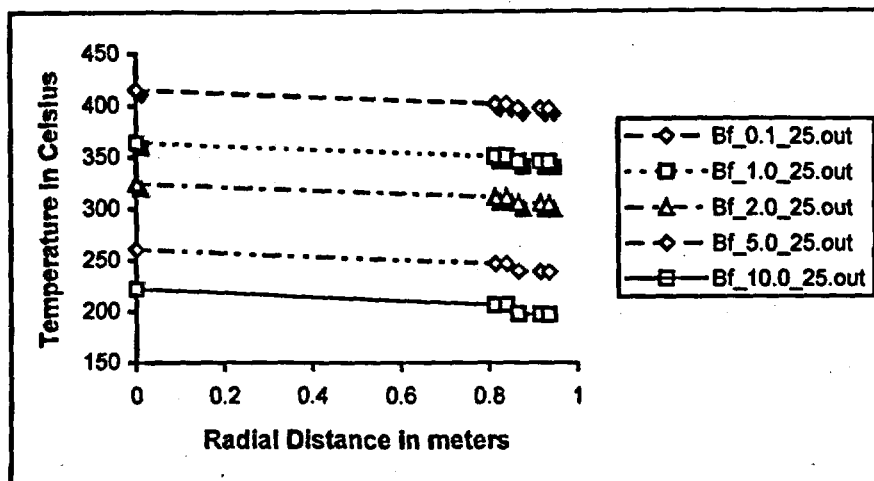


Figure 3. Temperature Versus Radial Distance for the Cases With Backfill (25-yr. ventilation)

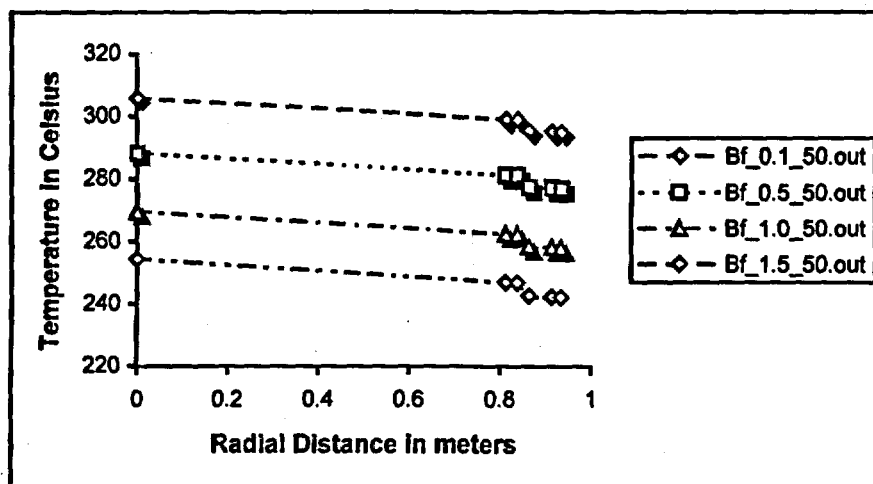


Figure 4. Temperature Versus Radial Distance for the Cases With Backfill (50-yr. ventilation)

7. ATTACHMENTS

The list of attachments is provided in Table 12.

Table 12. Attachments

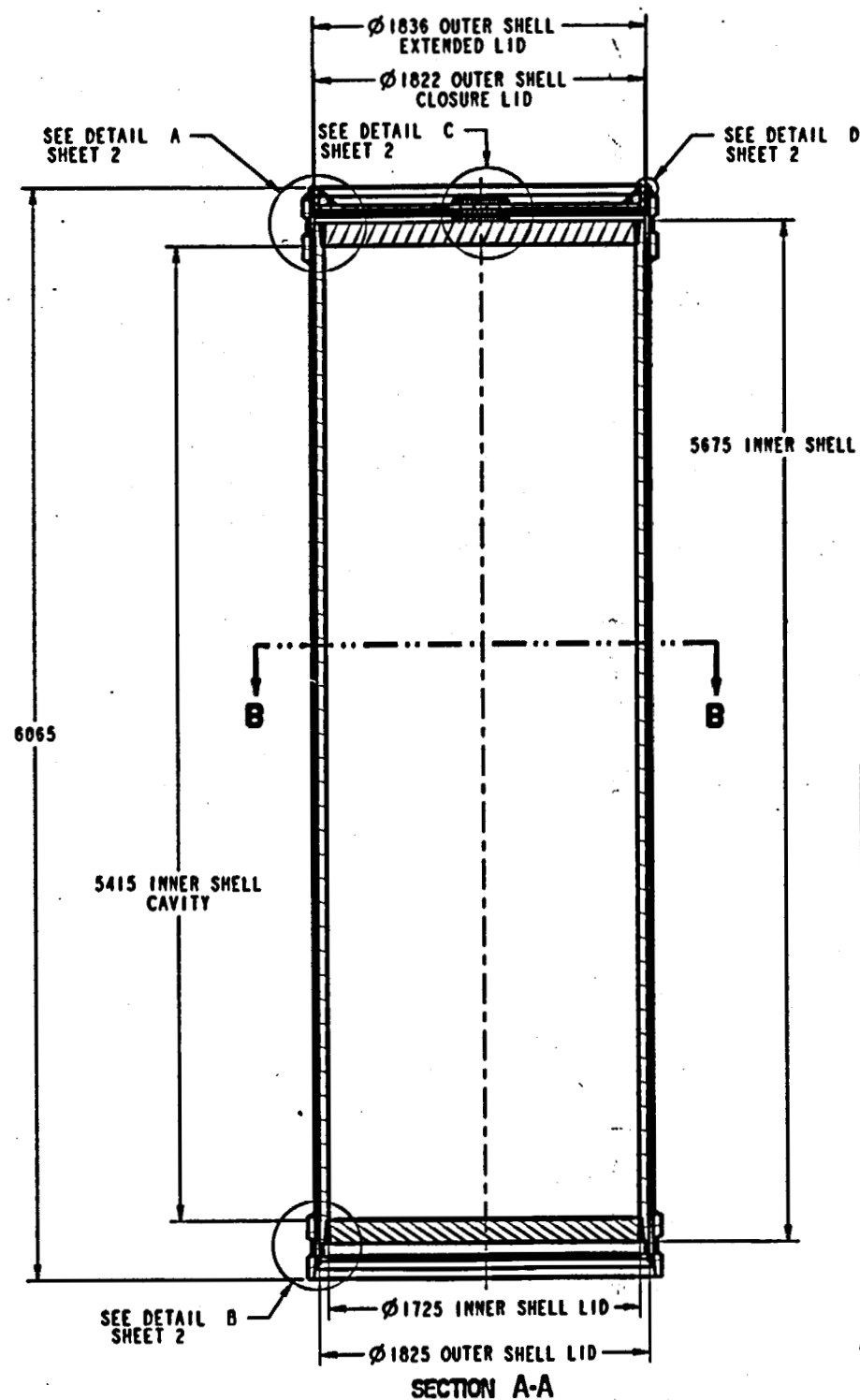
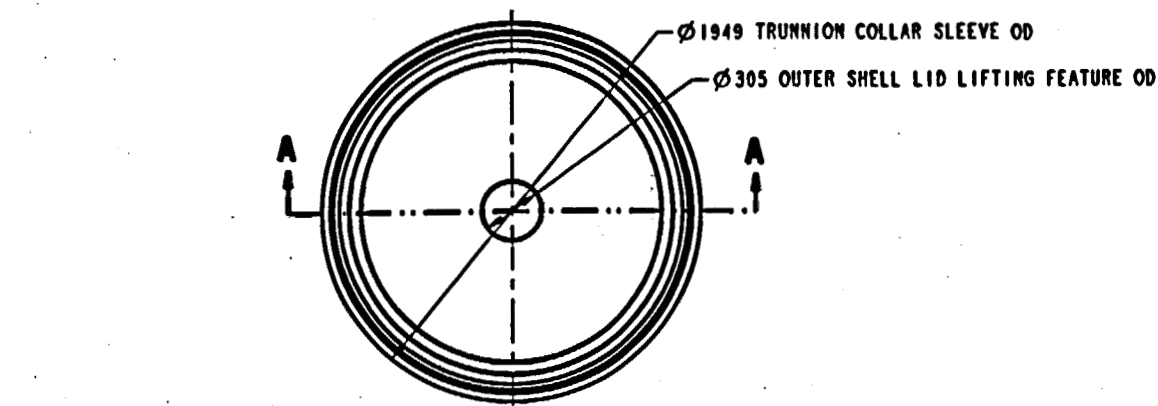
Attachment Number	Description	File Name	Size (pages)
I	Navy SNF Long Canister Configuration Sketch	SK-0194 REV 00	2
II	Material Properties File for ANSYS	Propnew03.dat	4
III	Document Input Reference System (DIRS) database Sheet	DIRS.doc	3
IV	21 PWR WP Surface Temperature File	Bf_0.1_25.parm	7
V	21 PWR WP Surface Temperature File	Bf_0.1_50.parm	8
VI	21 PWR WP Surface Temperature File	Bf_0.5_50.parm	8
VII	21 PWR WP Surface Temperature File	Bf_1.0_25.parm	7
VIII	21 PWR WP Surface Temperature File	Bf_1.0_50.parm	8
IX	21 PWR WP Surface Temperature File	Bf_1.5_50.parm	8
X	21 PWR WP Surface Temperature File	Bf_2.0_25.parm	7
XI	21 PWR WP Surface Temperature File	Bf_5.0_25.parm	7
XII	21 PWR WP Surface Temperature File	Bf_10.0_25.parm	7
XIII	21 PWR WP Surface Temperature File	NoBf_0.1_25.parm	7
XIV	21 PWR WP Surface Temperature File	NoBf_0.1_50.parm	8
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XVII	21 PWR WP Surface Temperature File	NoBf_1.0_50.parm	8
XVIII	21 PWR WP Surface Temperature File	NoBf_1.5_50.parm	8
XIX	21 PWR WP Surface Temperature File	NoBf_2.0_25.parm	7
XX	21 PWR WP Surface Temperature File	NoBf_5.0_25.parm	7
XXI	21 PWR WP Surface Temperature File	NoBf_10.0_25.parm	7
XXII	Heat Flux on the Surface of the Navy Canister	N/A	3

NOTE: N/A – Not Applicable

8. REFERENCES

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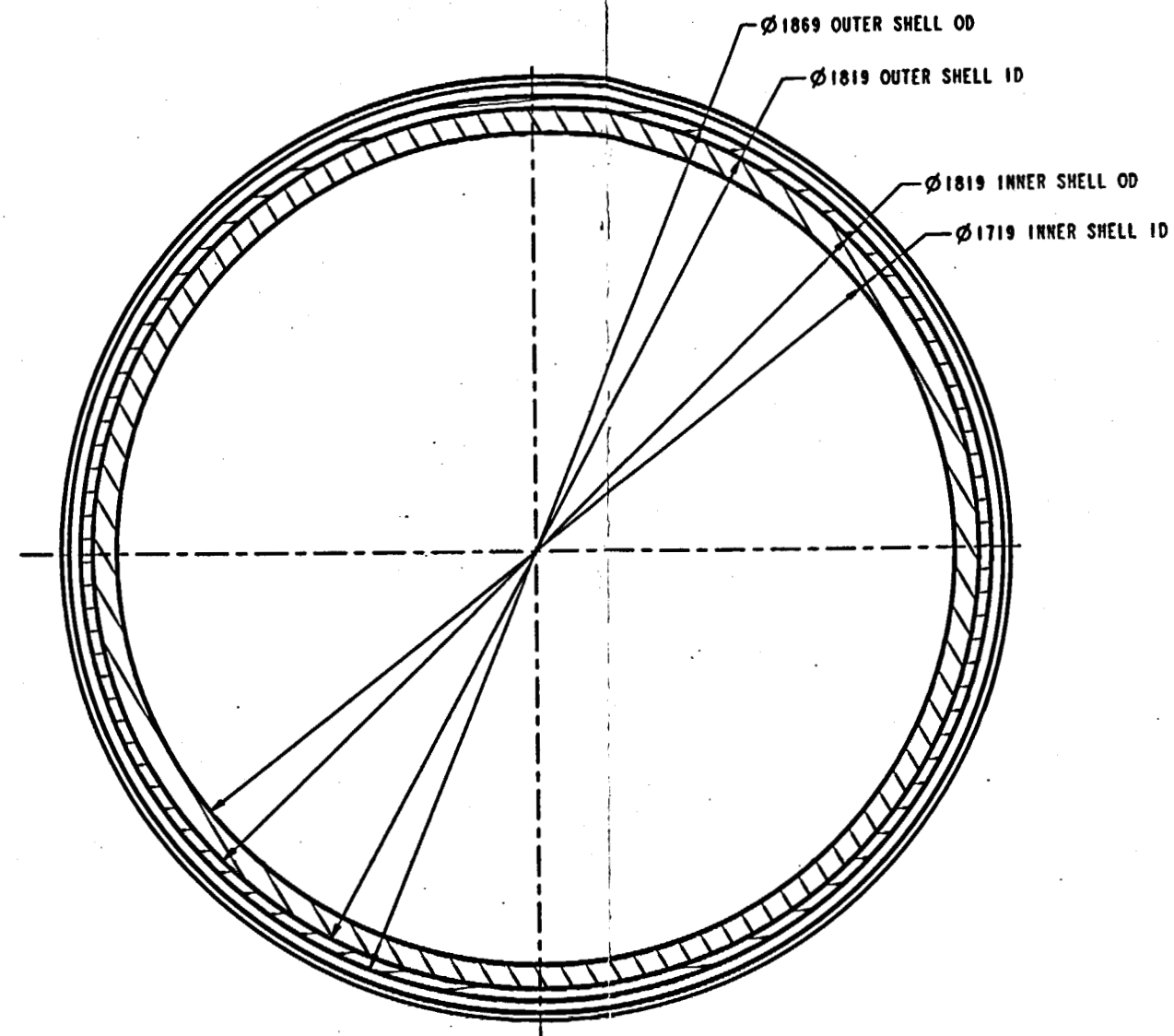
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OUTER SHELL	SB-575 N06022	25	7430	1
EXTENDED OUTER SHELL LID	SB-575 N06022	25	158	1
EXTENDED OUTER SHELL LID BASE	SB-575 N06022	25	528	1
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OUTER SHELL FLAT CLOSURE LID	SB-575 N06022	10	227	1
OUTER SHELL FLAT BOTTOM LID	SB-575 N06022	25	564	1
UPPER TRUNNION COLLAR SLEEVE	SB-575 N06022	40	604	1
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TOTAL 316 WELDS	SFA-5.9 S31600	-	243	**
WASTE PACKAGE ASSEMBLY	-	-	28005	1
NAVAL SNF	-	-	44452	1
WASTE PACKAGE WITH SNF	-	-	72457	1

**MAXIMUM EXPECTED PARAMETERS FOR NAVAL REACTORS CANISTERS* 10/29/97 FROM: RICHARD GUIDA
TO: RUSSELL DYER. MOL.19980121.0011

**REFER TO SK-0195 REV 00 "NAVAL SNF LONG WASTE PACKAGE WELD CONFIGURATION"

UNITS: mm

DO NOT SCALE FROM SKETCH



SECTION B-B

"FOR INFORMATION ONLY"

NAVAL SNF LONG WASTE PACKAGE CONFIGURATION
FOR SITE RECOMMENDATION

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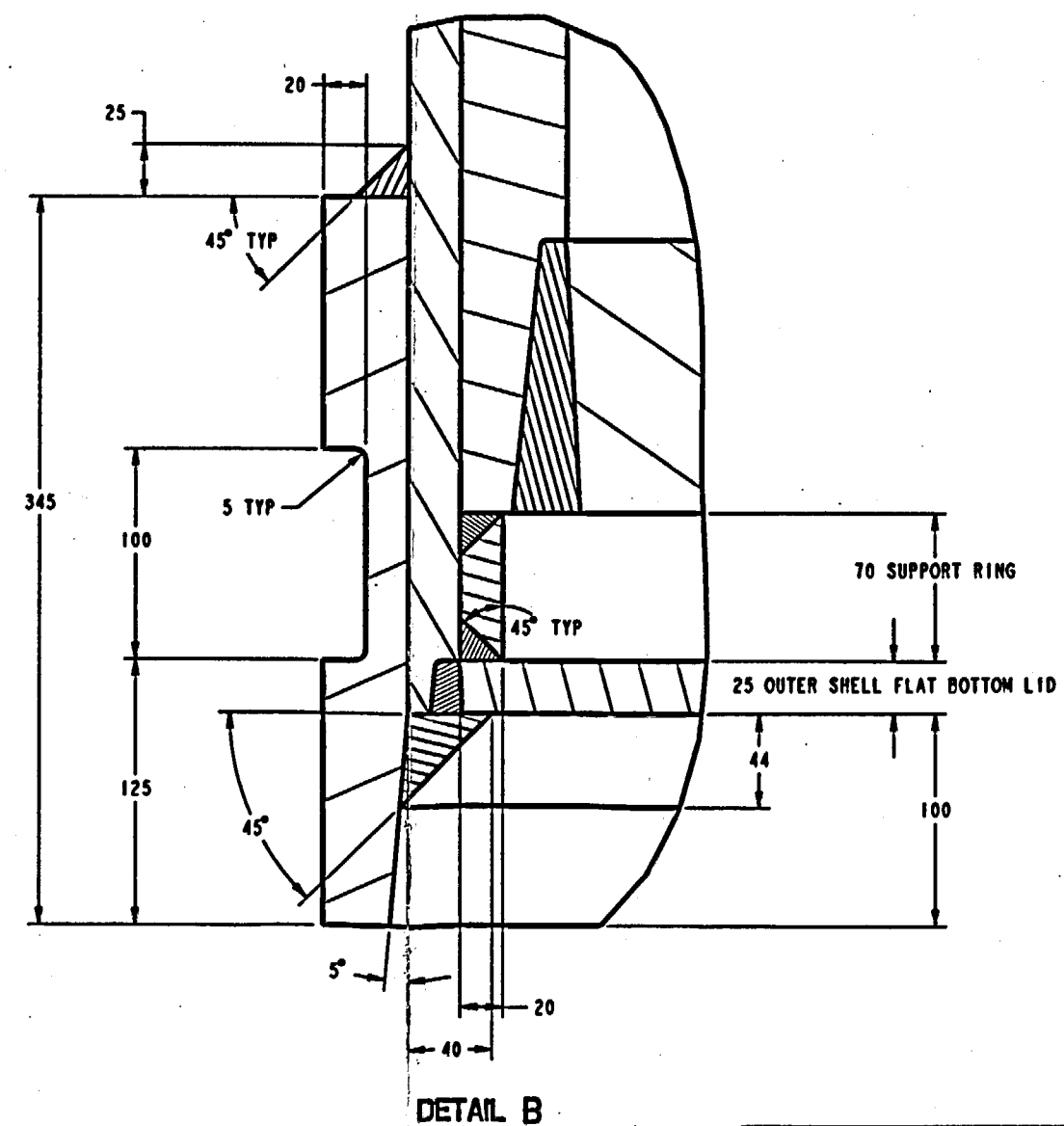
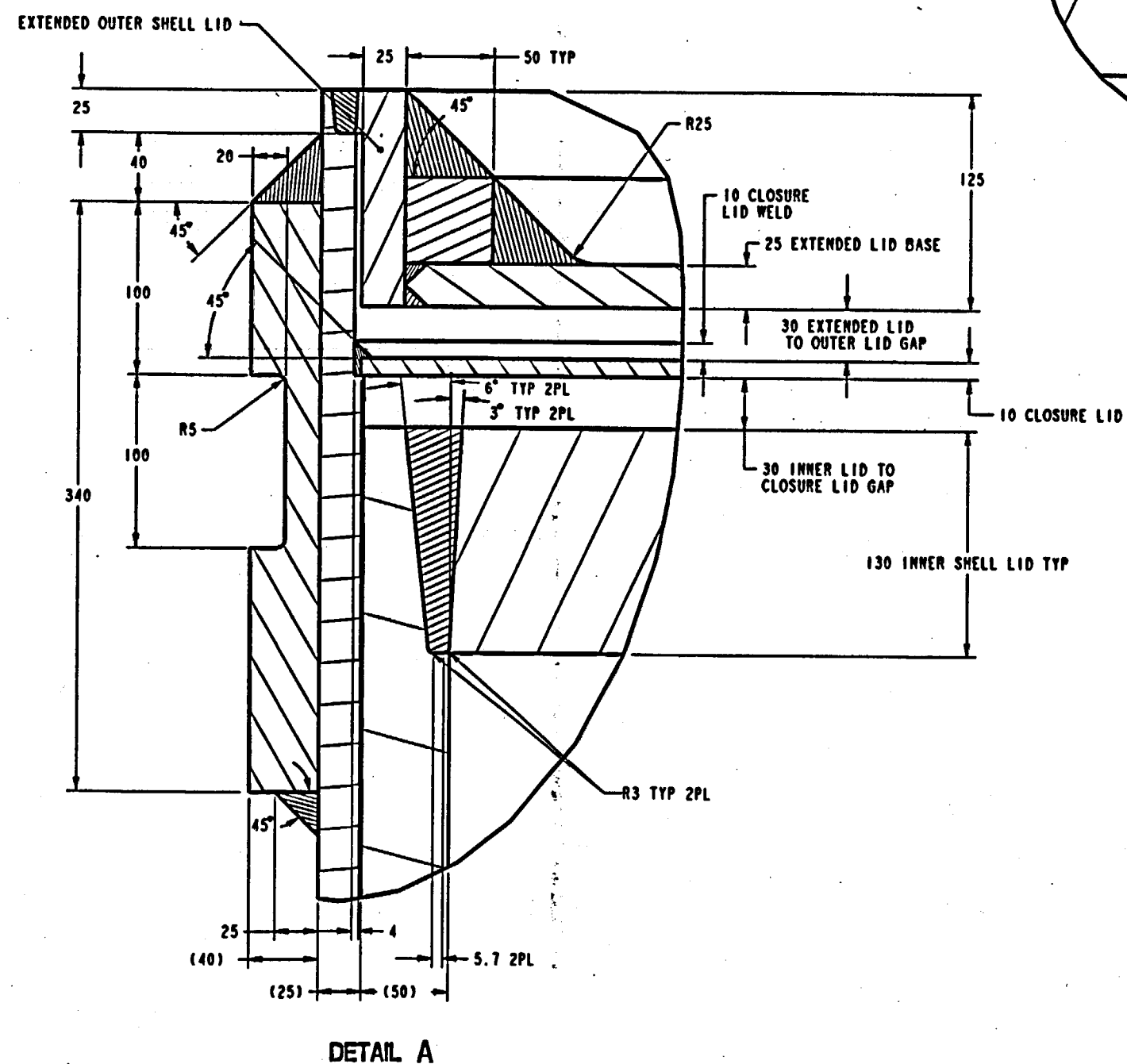
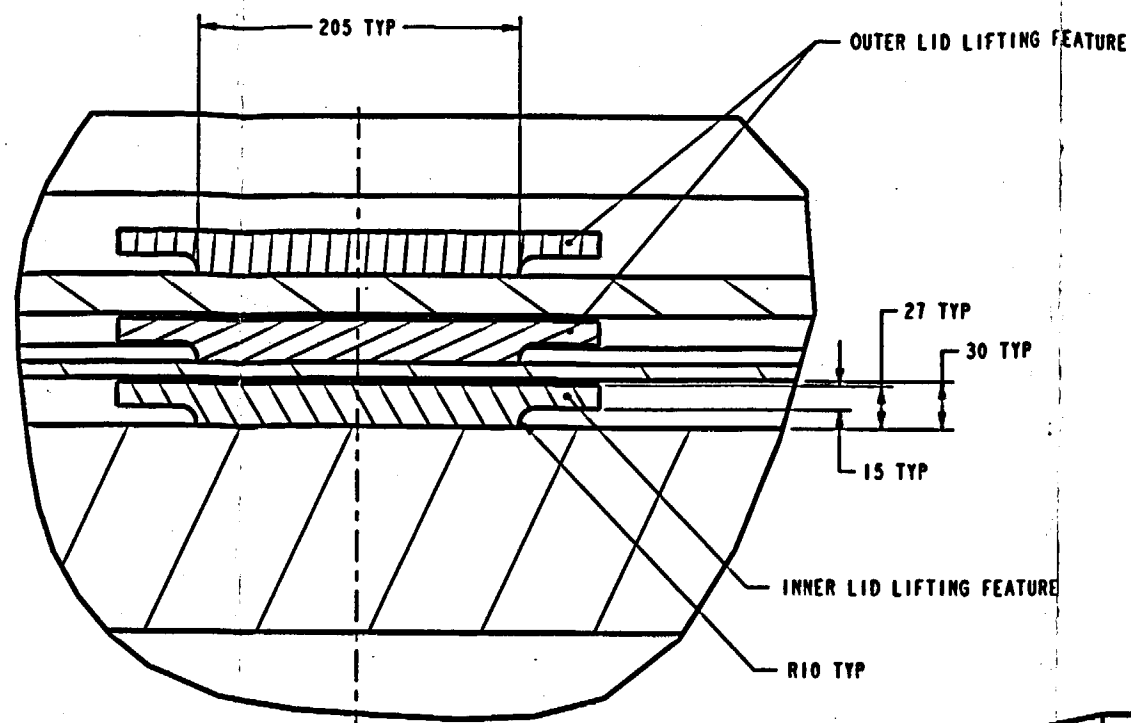
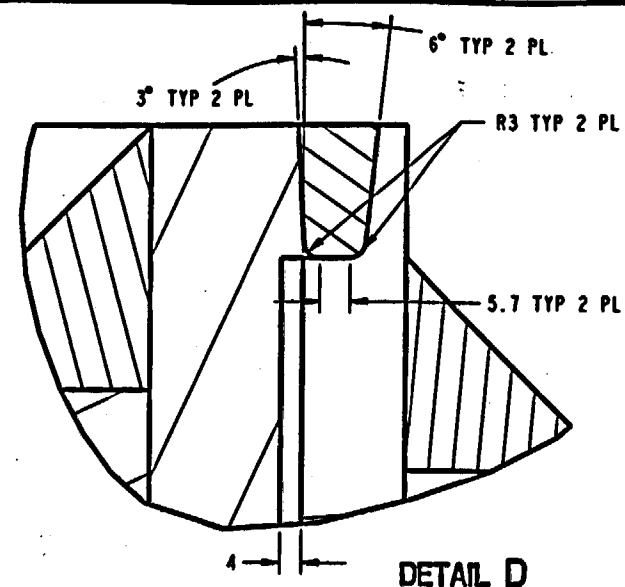
SHEET 1 OF 2

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DATE: 01/11/00

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OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT DOCUMENT INPUT REFERENCE SHEET									
1. Document Identifier No./Rev.: CAL-VDC-TH-000001 Rev. 00 (as of 25-apr-2000 08:30:51)			Change:		Title: THERMAL EVALUATION FOR THE NAVAL SNF WASTE PACKAGE				
Input Document			4. Input Status	5. Section Used in	6. Input Description	7. TBV/TBD Priority	8. TBVDue To		
2a.	2. Technical Product Input Source Title and Identifier(s) with Version	3. Section					Unqual.	From Uncontrolled Source	Un-Confirmed
1	Doering, T.W. 1998. "Qualification of ANSYS V5.4 on New WPO HP UNIX Workstation." Interoffice correspondence from T.W. Doering (CRWMS M&O) to G. Carlisle, November 11, 1998, LV.WP.MML.11/98-220. ACC: MOL.19981217.0106.	Entire	N/A - Reference Only	4.	Applicable workstations for ANSYS V5.4.	N/A	N/A	N/A	N/A
2	Doering, T.W. 1998. "Qualification of ANSYS V5.4 on the WPO HP UNIX Workstations." Interoffice correspondence from T.W. Doering (CRWMS M&O) to G. Carlisle, May 22, 1998, LV.WP.SMB.05/98-100. ACC: MOL.19980730.0147.	Entire	N/A - Reference Only	4.	Applicable workstation for ANSYS V5.4	N/A	N/A	N/A	N/A
3	CRWMS M&O 1998. <i>Controlled Design Assumptions Document</i> . B00000000-01717-4600-00032 REV 05. Las Vegas, Nevada: CRWMS M&O. ACC: MOL.19980804.0481.	pages 3-23 and 3-58	N/A - Reference Only	5.4	Horizontal emplacement of Waste Packages	N/A	N/A	N/A	N/A
4	CRWMS M&O 1998. <i>Software Qualification Report for ANSYS V5.4, A Finite Element Code</i> . CSCI: 30040 V5.4. DI: 30040-2003, Rev. 00. Las Vegas, Nevada: CRWMS M&O. ACC: MOL.19980609.0847.	Entire	N/A - Reference Only	4.	Software qualification report for ANSYS Version 5.4	N/A	N/A	N/A	N/A

5	Naples, E.M. 1999. Thermal, Shielding, and Structural Information on the Naval Spent Nuclear Fuel (SNF) Canister. Letter from E.M. Naples (Department of the Navy) to D.C. Haught (DOE/YMSCO), August 6, 1999, with enclosures. ACC: MOL.19991001.0133.	Pages 2 through 12	N/A - Qualified/Confirmed/Controlled	5.4	Thermal properties of Naval Spent Nuclear Fuel (SNF) canisters.	N/A	N/A	N/A	N/A
6	Bird, R.B.; Stewart, W.E.; and Lightfoot, E.N. 1960. <i>Transport Phenomena</i> . New York, New York: John Wiley & Sons. TIC: 208957.	Page 255	N/A - Reference Only	3.4	Statement regarding the pressure independence of thermal conductivities.	N/A	N/A	N/A	N/A
7	Knoll, R.W. and Gilbert, E.R. 1987. <i>Evaluation of Cover Gas Impurities and Their Effects on the Dry Storage of LWR Spent Fuel</i> . PNL-6365. Richland, Washington: Pacific Northwest Laboratory. TIC: 213789.	Page 4	N/A - Reference Only	3.4	Storage cask fill pressure.	N/A	N/A	N/A	N/A
8	Avallone, E.A. and Baumeister, T., III, ed. 1987. <i>Marks' Standard Handbook for Mechanical Engineers</i> . 9th Edition. New York, New York: McGraw-Hill. TIC: 206891.	Page 4-68	N/A - Accepted Data (Fact)	3.11, 5.2	Emissivity of 316 stainless steel	N/A	N/A	N/A	N/A
9	Incropera, F.P. and DeWitt, D.P. 1996. <i>Introduction to Heat Transfer</i> . 3rd Edition. New York, New York: John Wiley & Sons. TIC: 241057.	Page 759	N/A - Accepted Data (Fact)	5.2	Properties of Helium	N/A	N/A	N/A	N/A
10	Lide, D.R., ed. 1995. <i>CRC Handbook of Chemistry and Physics</i> . 76th Edition. Boca Raton, Florida: CRC Press. TIC: 216194.	page 10-297	N/A - Accepted Data (Fact)	5.2	Emissivity of Alloy-22	N/A	N/A	N/A	N/A
11	ASTM G 1-90 (Reapproved 1999). 1990. <i>Standard Practice for Preparing, Cleaning, and Evaluating Corrosion Test Specimens</i> . West Conshohocken, Pennsylvania: American Society for Testing and Materials. TIC: 238771.	Page 7	N/A - Accepted Data (Fact)	5.2	Density of 316 stainless steel	N/A	N/A	N/A	N/A

12	Haynes International 1997. <i>Hastelloy C-22 Alloy</i> . Kokomo, Indiana: Haynes International. TIC: 238121.	Page 13	N/A - Accepted Data (AMOPE approved)	5.2	Properties of Alloy-22	N/A	N/A	N/A	N/A
13	CRWMS M&O 2000. <i>Thermal Evaluation for the Naval SNF Waste Package</i> . TDP-VDC-TH-000001 REV 00. Las Vegas, Nevada: CRWMS M&O. ACC: MOL.20000107.0057.	Entire	N/A - Reference Only	1.	Technical Development Plan	N/A	N/A	N/A	N/A
14	CRWMS M&O 2000. <i>Electronic Files for Thermal Evaluations for the Naval SNF Canister</i> . CAL-VDC-TH-000001 REV 00. Las Vegas, Nevada: M&O. ACC: MOL.20000131.0352.	entire	TBV-4131	entire	ROCK LAYER LOCATIONS AND PROPERTIES	3	X	N/A	N/A
15	ASME (American Society of Mechanical Engineers) 1995. "Materials." Section II of <i>1995 ASME Boiler and Pressure Vessel Code</i> . New York, New York: American Society of Mechanical Engineers. TIC: 245287.	Page 606	N/A - Accepted Data (Fact)	5.2	Thermal conductivity and thermal diffusivity of stainless steel 316	N/A	N/A	N/A	N/A
16	CRWMS M&O 2000. <i>Drift Scale Thermal Analysis</i> . CAL-WIS-TH-000002 REV 00. Las Vegas, Nevada: M&O. ACC: MOL.20000420.0401.	Attach: I-X, XIII-XX	TBV-4131	5	ROCK LAYER LOCATIONS AND PROPERTIES	3	X	N/A	N/A

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Heat Flux on the Surface of the Navy Canister

A hand calculation has been performed to determine the heat flux on the surface of the navy canister. The calculation was repeated for several time steps measured from the initial time of waste package emplacement. The heat transfer due to convection was considered insignificant on the basis of the extremely small convection cell. The peak temperature present on the surface of the navy canister and the cavity wall of the waste package was assumed uniform over their respective surfaces. The peak temperatures were taken from ANSYS calculations. The ANSYS calculation considered the current design of the repository (0.1-m waste package gap, 25 yrs. of ventilation, and no backfill). The radiation heat transfer was calculated in two dimensions (2-D) for concentric cylinders (Reference 8.11, p. 699):

$$q'' = \frac{\sigma \cdot (T_s^4 - T_{wp}^4)}{\frac{1}{\epsilon_s} + \frac{1 - \epsilon_{wp}}{\epsilon_{wp}} \cdot \left(\frac{r_s}{r_{wp}} \right)} \quad (\text{Equation 1})$$

Where σ represents the Stefan-Boltzmann constant of $5.67 \times 10^{-8} \text{ W} \cdot \text{m}^{-2} \cdot \text{K}^{-4}$, T_s is the surface temperature of the navy canister, T_{wp} is the temperature present on the wall of the waste package cavity, ϵ_s is 0.6 the emissivity of the navy canister, ϵ_{wp} is 0.6 the emissivity of the inner shell of the waste package, r_s is 0.8382 meters and represents the radius of the navy canister, r_{wp} is 0.8595 meters and represents the cavity radius of the waste package.

The conduction heat transfer was calculated in one dimension for a 1-inch plane wall of helium (Reference 8.11, p. 5).

$$q'' = k \frac{T_s - T_{wp}}{L} \quad (\text{Equation 2})$$

Where k is the thermal conductivity of helium at 160° C (2.013 W/m°k), and L is the distance from the navy canister surface to the cavity wall (0.0213 meters).

The time steps, navy canister surface temperature at each time step, and cavity wall temperature at each time step are enumerated in Table 1.

The time steps, navy canister surface temperature at each time step, and heat flux present on the surface of navy canister at each time step are presented in Table 2.

Table 1 Inputs for Heat Transfer Hand Calculation

Time Since Emplacement (years)	Navy Canister surface Temp. (Celsius)	Waste Package Cavity Wall Temp. (Celsius)	Time Since Emplacement (years)	Navy Canister surface Temp. (Celsius)	Waste Package Cavity Wall Temp. (Celsius)
0	92.4217	64.4047	50	230.408	226.096
0.000001	92.4217	64.4047	60	219.932	216.314
0.1	108.147	82.1888	70	209.804	206.784
0.2	112.174	86.5978	80	200.642	198.133
0.3	114.43	89.31	90	192.852	190.776
0.4	116.06	91.3432	100	186.747	185.029
0.5	117.343	92.9942	200	157.243	156.933
0.6	118.407	94.3982	300	143.561	143.41
0.7	119.296	95.6022	400	137.037	136.892
0.8	120.049	96.6579	500	132.162	132.02
0.9	120.697	97.5938	600	128.046	127.909
1	121.252	98.4282	700	124.491	124.358
2	124.736	103.707	800	121.451	121.319
3	126.148	106.328	900	118.757	118.63
4	126.807	107.857	1000	116.611	116.485
5	127.038	108.824	2000	98.9406	98.8223
6	126.959	109.361	3000	92.2433	92.1293
7	126.745	109.661	4000	87.3402	87.2256
8	126.398	109.753	5000	83.72	83.6048
9	125.994	109.724	6000	80.5371	80.4214
10	125.548	109.588	7000	78.105	77.9889
20	118.529	105.378	8000	76.0216	75.9027
30	229.258	222.558	9000	73.4987	73.3818
40	238.14	232.933	10000	71.3746	71.2548

Table 2 Results of the Hand Calculation

Time Since Emplacement (years)	Navy Canister surface Temp. (Celsius)	Heat Flux At the Surface of the Navy Canister (W/m ²)	Time Since Emplacement (years)	Navy Canister surface Temp. (Celsius)	Heat Flux At the Surface of the Navy Canister (W/m ²)
0	92.4217	384.1443	50	230.408	93.9619
0.000001	92.4217	384.1443	60	219.932	76.1874
0.1	108.147	372.4492	70	209.804	61.5325
0.2	112.174	371.3128	80	200.642	49.6276
0.3	114.43	367.2457	90	192.852	40.0483
0.4	116.06	363.2262	100	186.747	32.5039
0.5	117.343	359.3103	200	157.243	5.3465
0.6	118.407	355.5391	300	143.561	2.4961
0.7	119.296	351.9233	400	137.037	2.3495
0.8	120.049	348.3266	500	132.162	2.2671
0.9	120.697	344.8204	600	128.046	2.1604
1	121.252	341.3295	700	124.491	2.0751
2	124.736	318.4884	800	121.451	2.0411
3	126.148	301.9394	900	118.757	1.9482
4	126.807	289.6056	1000	116.611	1.9208
5	127.038	278.8422	2000	98.9406	1.7143
6	126.959	269.5891	3000	92.2433	1.6216
7	126.745	261.7451	4000	87.3402	1.6084
8	126.398	254.9214	5000	83.72	1.6010
9	125.994	249.0180	6000	80.5371	1.5943
10	125.548	244.0634	7000	78.105	1.5895
20	118.529	197.8341	8000	76.0216	1.6189
30	229.258	144.8464	9000	73.4987	1.5812
40	238.14	116.3066	10000	71.3746	1.6115